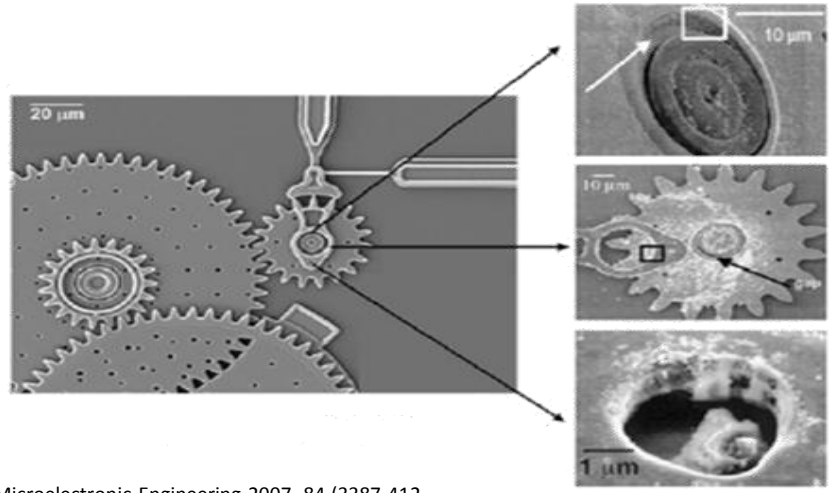
Studies on the Use of Atomically Thin Films for Controlling Friction and Adhesion at Interfaces

Bradley Ewers, Jessica Spear, James Custer,† Meagan Elinski and James Batteas
Departments of Chemistry and Materials Science and Engineering, Texas A&M University, College Station, TX 77843

The Batteas Research Group

Introduction

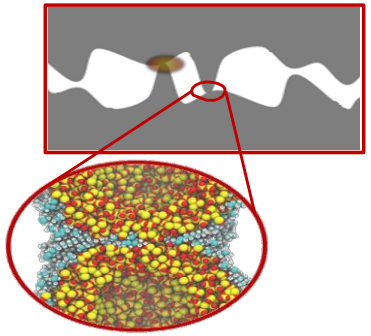
Wear and energy dissipation resulting from friction between interfaces represents an enormous cost to society, approximately 1.5% of global GDP (~$200 billion annually in the U.S.) is lost due to surface wear and energy inefficiency. Furthermore, demanding applications like Microelectromechanical systems devices (MEMS) and space-based applications represent unique lubrication challenges that require the absolute best performance from surface coatings and lubricants. Understanding the atomic and molecular origins of friction and lubrication is therefore essential to overcoming these challenges and effectively controlling surface forces.

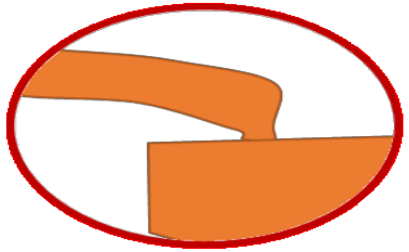


Microelectronic Engineering 2007, 84 (3387-412.

Due to their small size, restoring forces of MEMS devices are often insufficient to overcome surface forces like friction and adhesion, or the viscous drag associated with traditional lubricants. They represent one of the most challenging modern lubrication challenges.

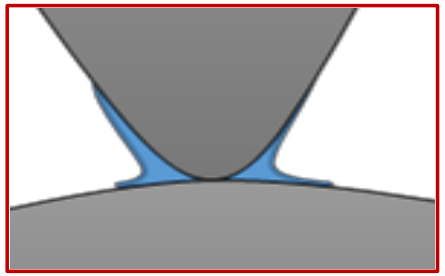
Tribochemistry at high pressure asperity interactions



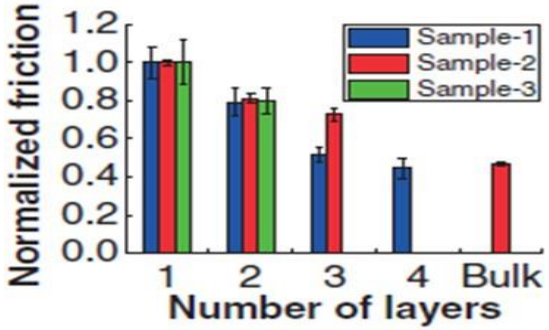


Cold welding of metallic contacts

Capillary condensation at hydrophilic interfaces



In real tribological interfaces, the contact between sliding surfaces is often not atomically smooth. When polysilicon is used during MEMS fabrication, device surfaces typically exhibit nanoscale roughness on the order of 10 nm. It is critical for device operation and longevity that these asperities resist wear. Asperities between the surfaces interact with each other during contact and the high pressures formed at these asperity-asperity contacts dominate the adhesion, friction, and wear between the surfaces. To control adhesion and friction, surface lubricants such as self- assembled monolayers and 2D materials like graphene are ideal to reduce capillary condensation as well as reduce the friction at the interface. Graphene is also mechanically strong and can withstand high pressure contacts but easily delaminates from the surface known as "puckering". A detailed understanding of the mechanisms of these materials on rough surfaces is still needed to aid in optimizing and controlling the surface interactions for long lasting friction and wear reduction.



Science 2010, 328 (5974), 76-80. 4

Much of the computation done for this research involved 256-way runs on the Eos cluster of the Texas A&M Supercomputing Facility using the LAMMPS MD software.

J.C. Spear, B.W. Ewers and J.D. Batteas, "2D-Nanomaterials for Controlling Friction and Wear at Interfaces," **10** *Nano Today* (2015) 301-314.

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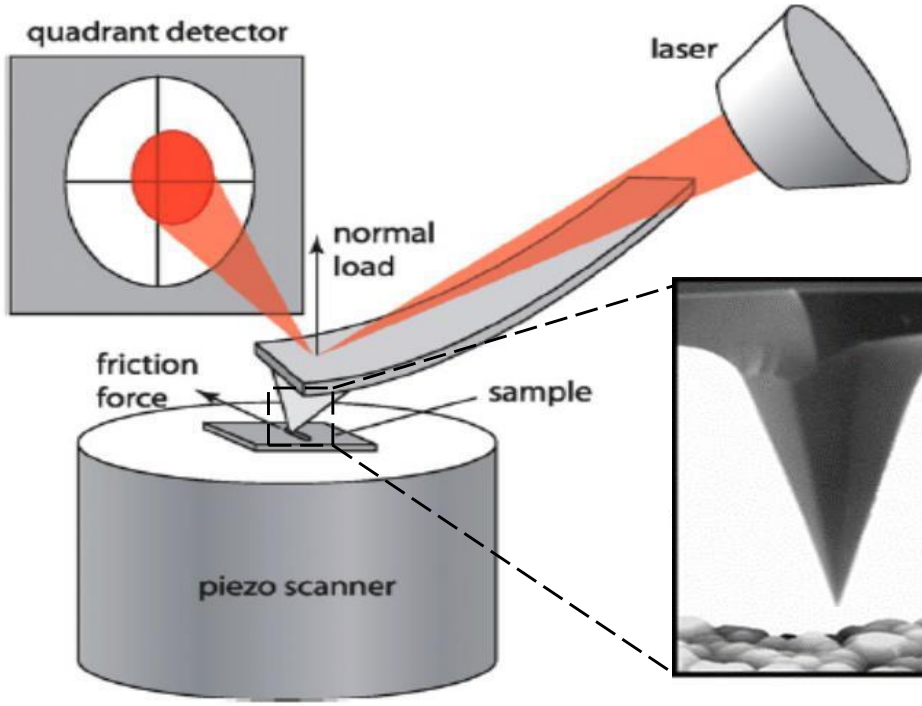
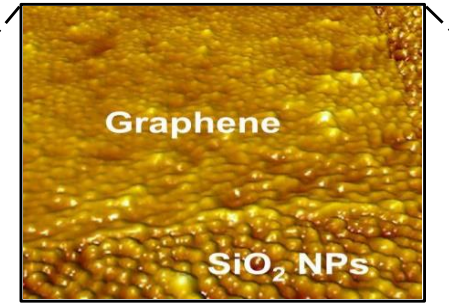
Experimental Measurements

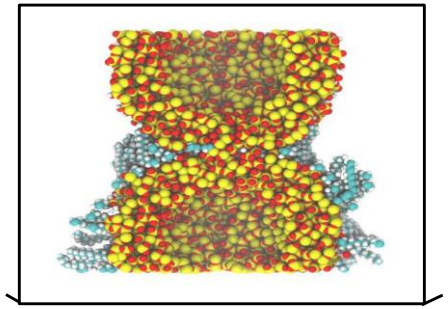


Journal of Physics D, 2008, 41 (12), 123001

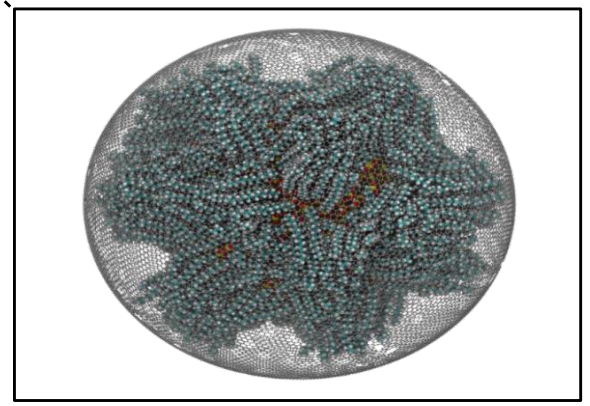
Atomic Force Microscopy

Asperity – Asperity Contacts





- ***High resolution surface imaging***
- ***Correlated friction and adhesion mechanics***



- ***Atomically detailed structure and dynamics***
- ***Isolation of key factors and variables***

Theoretical Calculations

To understand friction in atomically thick lubricants like graphene, a complete understanding of the structure and dynamics of these materials in sliding contacts is essential. To achieve this, we use Atomic Force Microscopy (AFM), complemented with atomistic Molecular Dynamics (MD) simulations. The high resolution measurement of surface forces like adhesion and friction that can be achieved with the AFM allows us to identify the critical phenomena which dictate the friction response of graphene, and through modeling and simulation we can identify the underlying mechanisms of these phenomena and how they are influenced by properties of the substrate and the graphene sheet.

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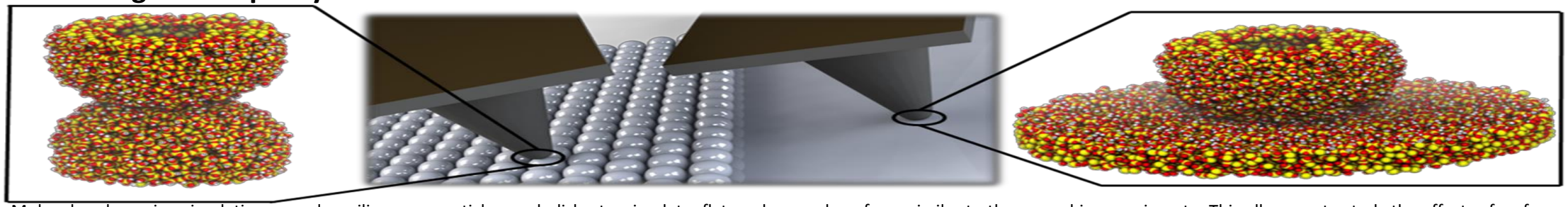
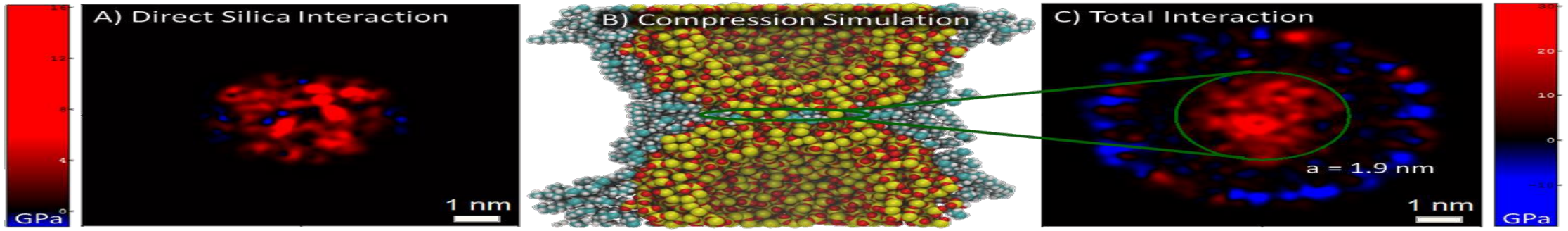
Modeling Contact and Sliding of Thin Films

Simulating Nanoasperity Contacts



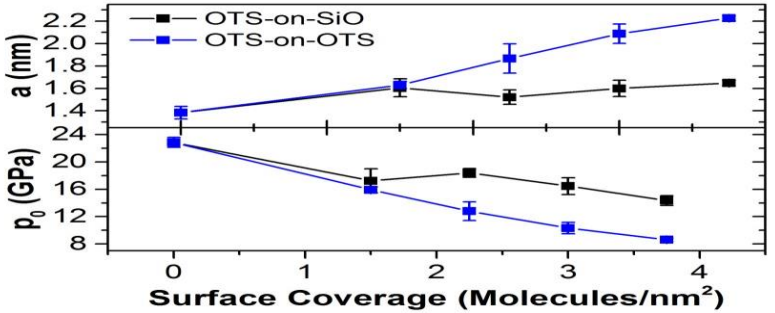
Molecular dynamics simulations employ silica nanoparticles and disks to simulate flat and curved surfaces similar to those used in experiment. This allows us to study the effects of surface morphology on the contact and friction response of surface coatings and boundary lubricants.

Contact Stress and Strain Analysis



Simulation Setup Video

Pressure and strain mapping routines have been developed to determine in atomistic detail the distribution of these properties. Furthermore, it allows us to track the evolution of these properties with increasing lubricant density or changes in lubricant properties and configuration. For example, the evolution of contact area and peak stress can be evaluated as a function of film density on surfaces.



B.W. Ewers and J.D. Batteas, "Utilizing Atomistic Simulations to Map Pressure Distributions and Contact Areas in Molecular Adlayers within Nanoscale Surface-Asperity Junctions: A Demonstration with Octadecylsilane Functionalized Silica Interfaces," *Langmuir* **30** (2014) 11897-11905.

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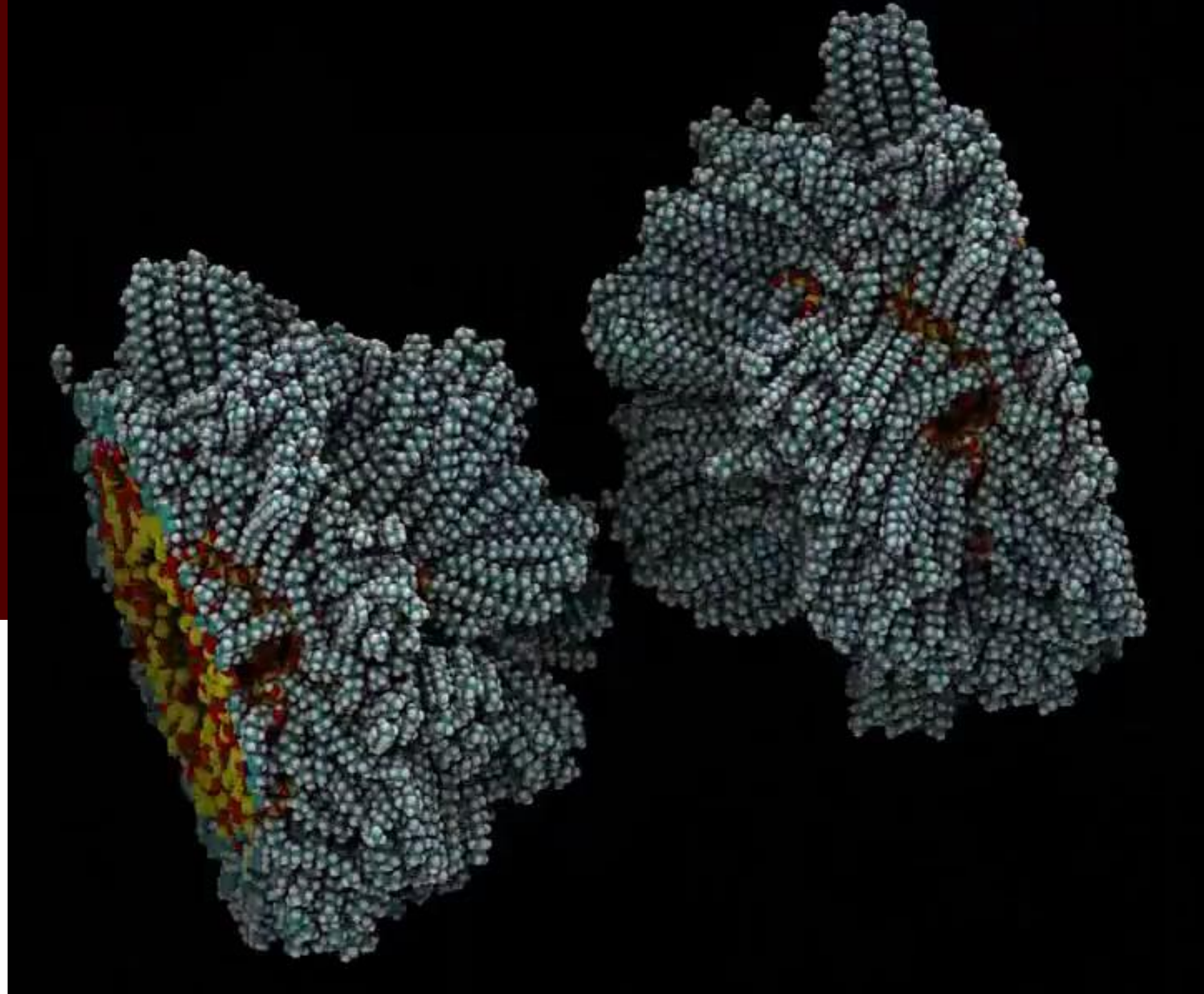
System Setup Animation



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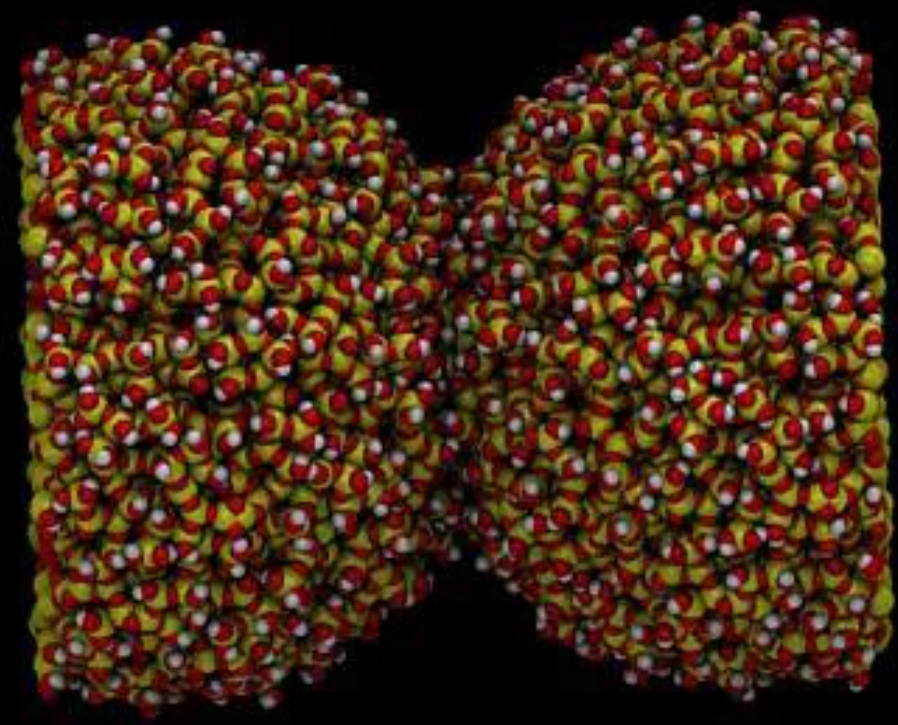
Bare Contact Simulation



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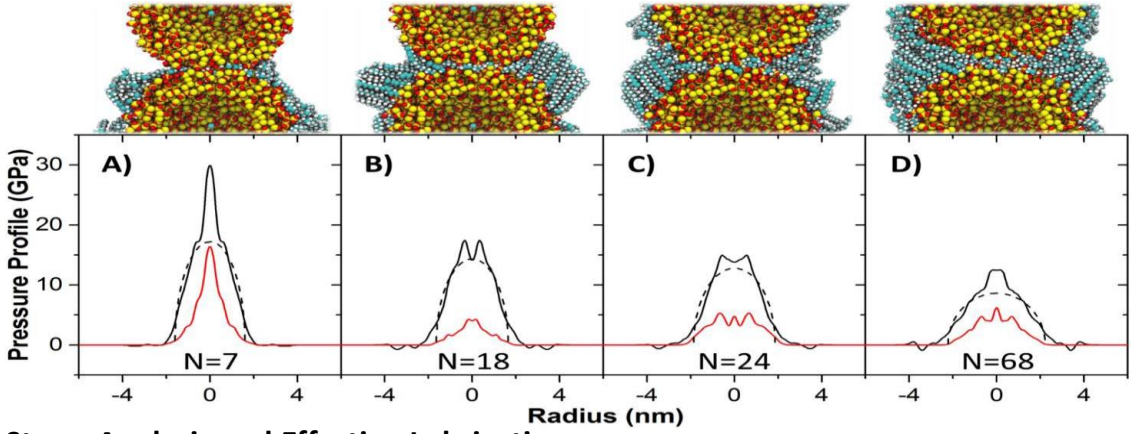
Modeling Contact and Sliding of Thin Films

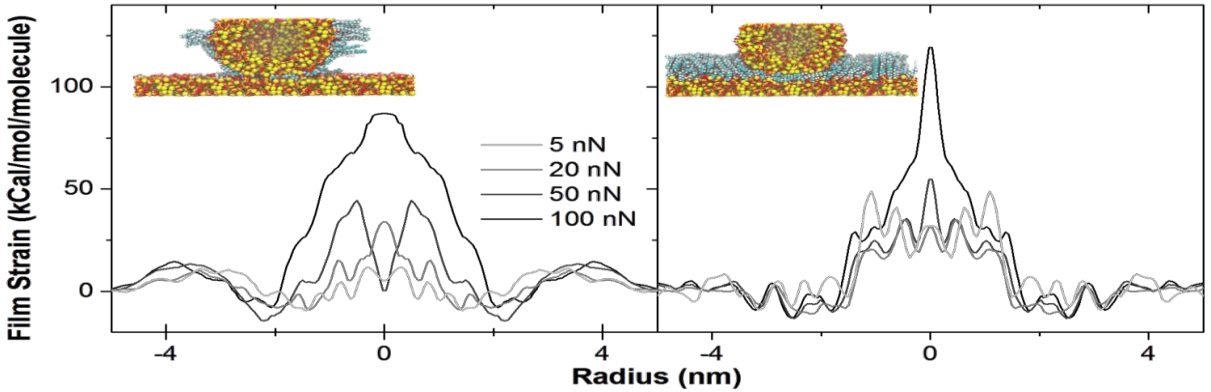


Stress Analysis and Effective Lubrication

Evaluation and decomposition of contact stresses between stresses imposed on the lubricant and the substrate can be used to guide the development of effective lubrication schemes. An effective lubricant should eliminate contact stresses at the substrate interface, minimizing pressure catalyzed tribochemistry and mechanical coupling of the sliding interfaces.

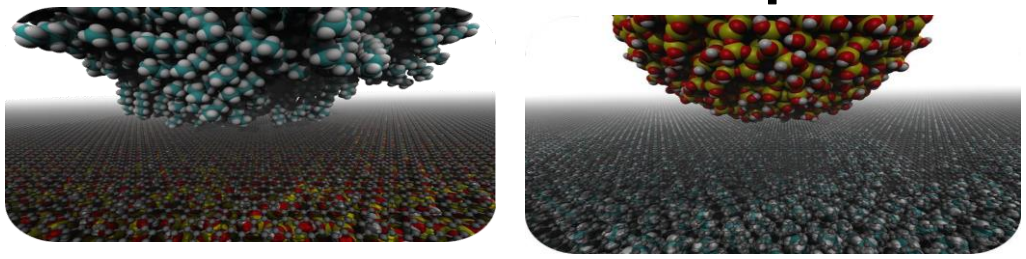
Strain Analysis and Tribochemical Wear

Isolating and evaluating strain in the lubricant film provides a guide to the point at which substantial tribochemistry can occur. For the OTS films considered here, the chemical bonds binding the molecules to the substrate have strengths of ~130 kCal/mol. Localization of the film strain at these magnitudes measured in simulations correlates with observation of wear in these lubricant films by AFM microscopy.



B.W. Ewers and J.D. Batteas, "The Role of Substrate Interactions in the Modification of Surface Forces by Self-assembled Monolayers," *RSC Advances* **4** (2014) 16803-16812.

Atomic Mechanisms of Friction in Graphene Films

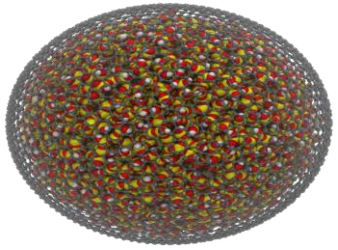


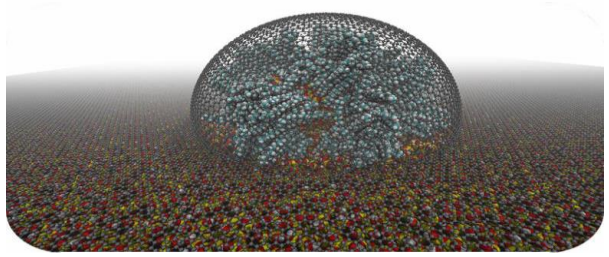
Surface Chemistry and Mechanics

The contact and sliding dynamics of graphene fundamentally depends on the interactions it has with the sliding interfaces. By varying the chemistry, morphology, and rigidity of the graphene's shearing and fixed interfaces, we can achieve a better understanding of how these interactions influence the behavior of graphene. Understands effects like puckering and wrinkling is possible, and the contribution of these effects to frictional dissipation can be isolated.

Friction of Graphene in Curved Geometries

We use two models of graphene on curved surfaces. Consistent with prior studies, a nanoparticle is used to simulate the nanoasperity morphology. The graphene sheet is applied either as a spherical structure with defects that alleviate curvature strain, or as typical graphene sheet placed across a nanoasperity. Comparison of these two situations isolates the influence of curvature strain on the friction dynamics and strain evolution in these materials under contact.





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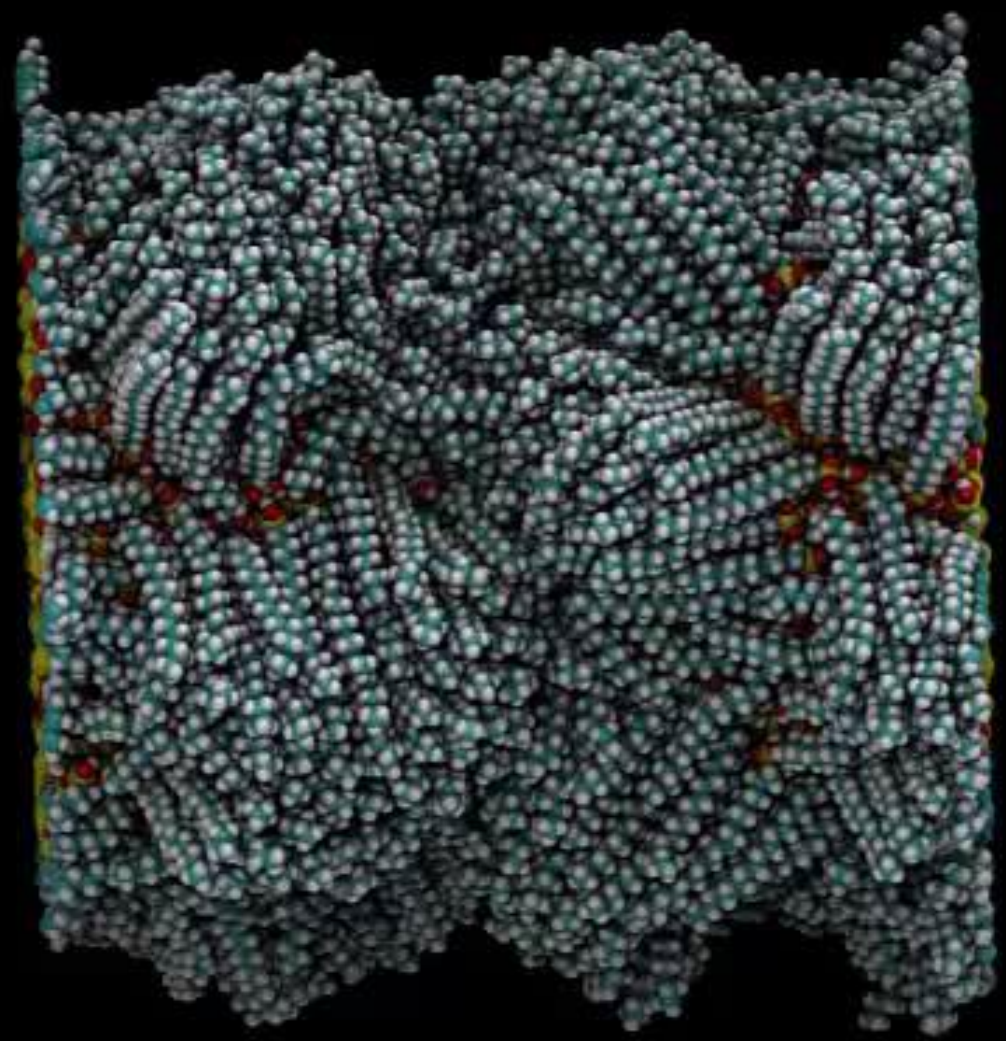
High Film Density Contact Simulation



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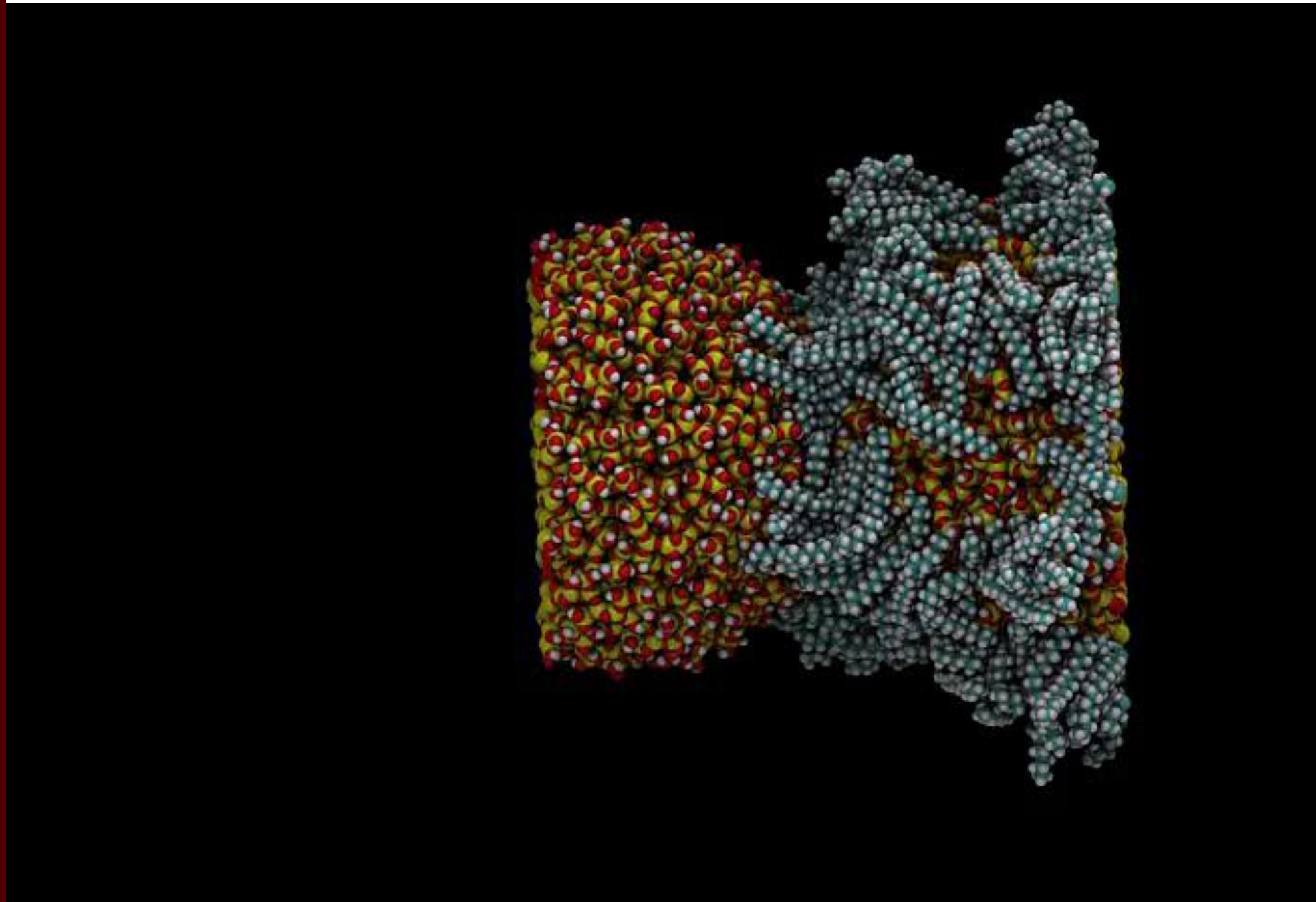
Low Film Density Contact Simulation



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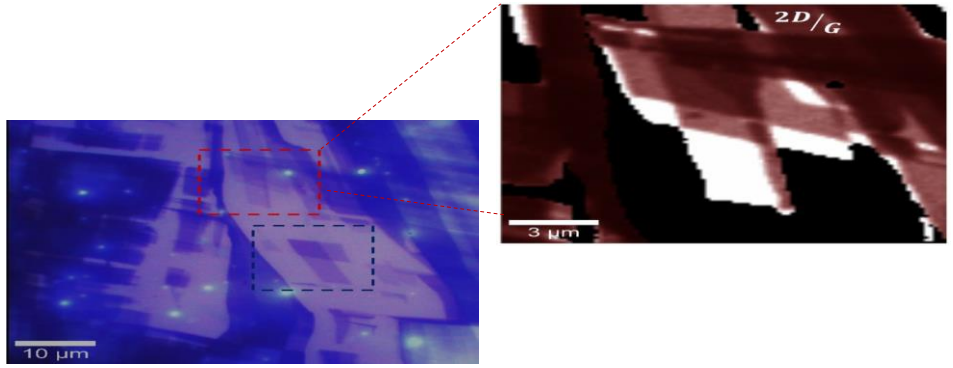
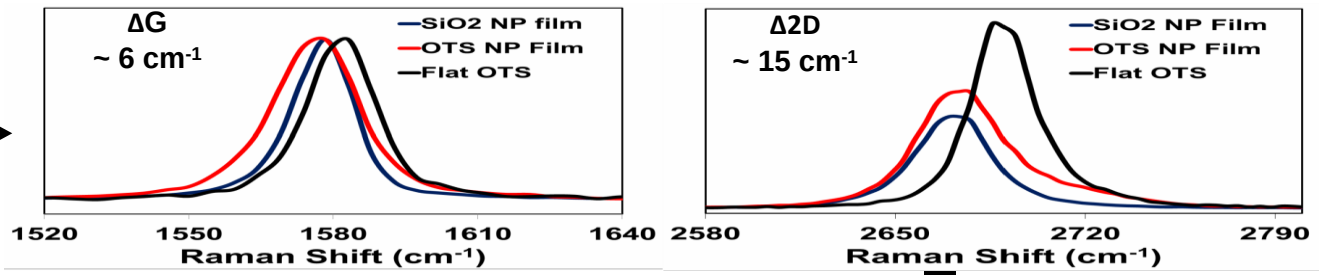
Friction and Adhesion of Graphene on Rough Surfaces

Raman Mapping & Strain Analysis



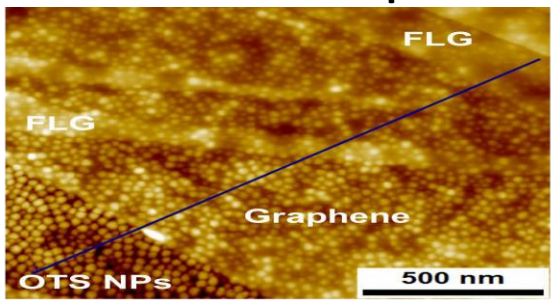
Due to sharp nanoparticle asperities the graphene is strained

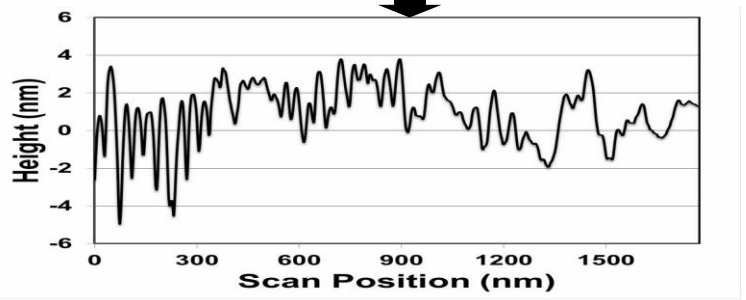


Analysis of the Raman spectra revealed small peak shifts attributed to biaxial strain in the graphene lattice due to the nanoscale roughness of the substrate as compared to graphene flakes on flat surfaces.

As layer thickness increases the bending stiffness also increases which results in a gradual reduction in the conformity and surface roughness as seen in the topography and line profile.

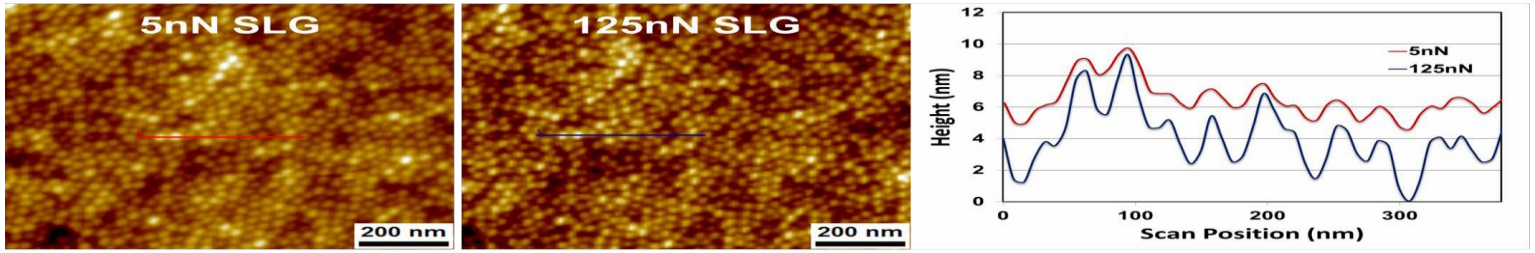
Surface Structure of Graphene Films





Graphene layers partially conform to nanoparticle substrates

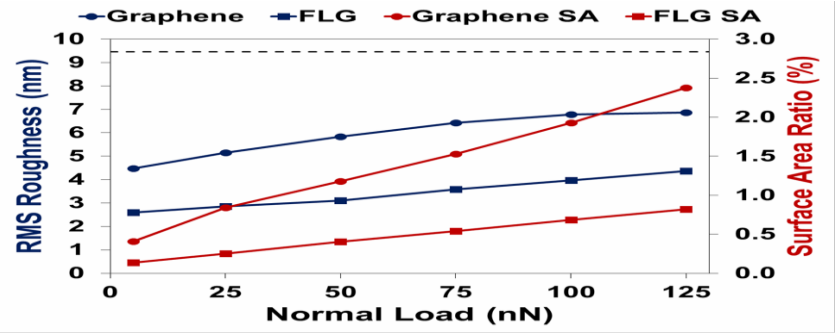
Effect of Mechanical Loading



Conformity increases under increasing applied load

When external force is applied with the AFM tip, the conformity of the graphene flakes reversibly increased which can be seen in the increased roughness at higher loads. The roughness maximized at ~6.5 nm indicating full conformity (~9.5 nm) is not achieved due to the large strain requirement of the substrate geometry.

Topography images for single and few layer graphene both showed increased roughness with larger loads, however, comparison of the line profiles indicated graphene is stretched 1-2 nm more than the few-layer graphene.



J.C. Spear, J.P. Custer and J.D. Batteas, "The Influence of Nanoscale Roughness and Substrate Chemistry on the Frictional Properties of Single and Few Layer Graphene," *Nanoscale* **7** (2015) 10021-10029.

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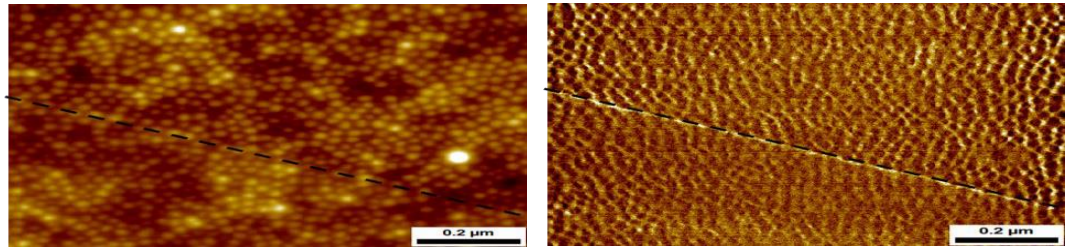
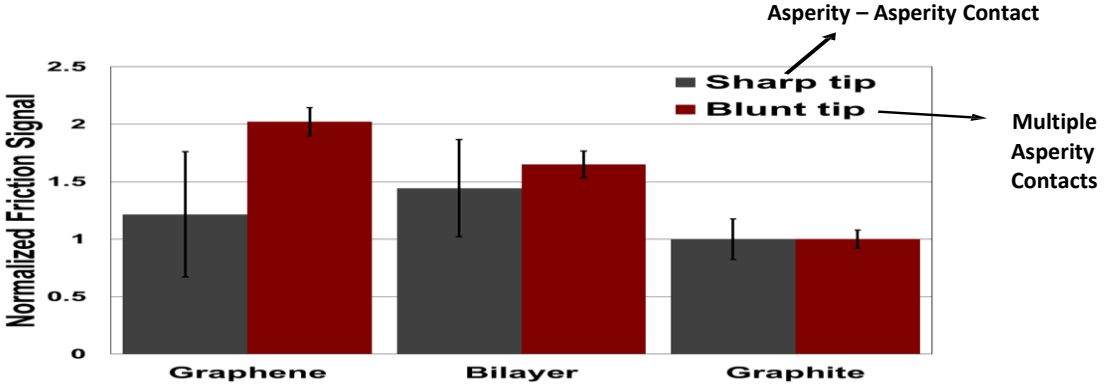
Hydrophilic Rough Surfaces

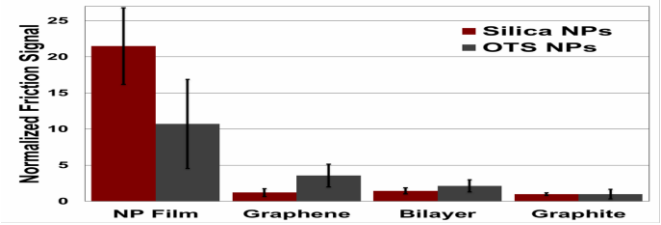


Suppression of the "puckering effect" between sharp asperities

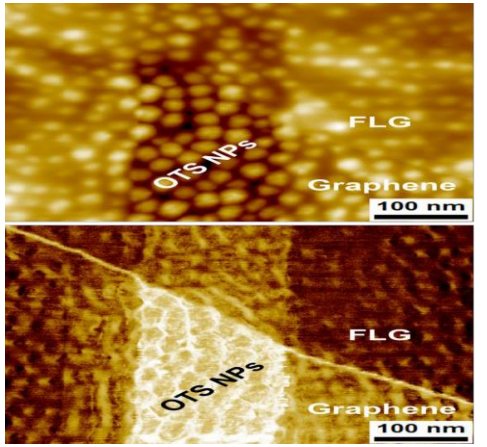


Using a sharp AFM probe (~ 30 nm radius) there is not a significant change in friction between the graphene layers and bulk-like graphene, however, with a blunt probe (~ 130 nm) much larger than the asperities, the friction on graphene is 50% higher than the bulk. This implies a contact area dependence where the larger probe has a larger adhesion to the graphene over the surface as compared to the smaller probe.

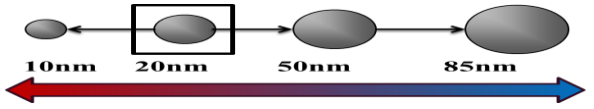
Hydrophobic Surface Interactions

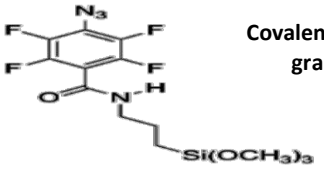


A significant contrast between the Nano-particles modified with Octadecyltrichlorosilane (OTS) and graphene layers can be easily seen in the AFM image. In this case, the friction was not found to depend on the contact area of the probe.



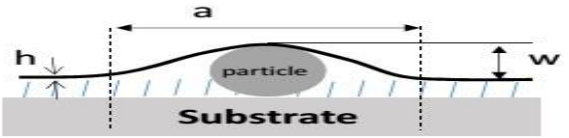
Outlook





Covalently binding graphene

Measuring graphene- substrate adhesion



Acknowledgements

We acknowledge the Texas A&M High Performance Research Computing (http://sc.tamu.edu/) for providing computing resources useful in conducting the research reported here, as well as the Texas A&M Laboratory for Molecular Simulation for advising and assisting in the use of these resources. We also acknowledge the assistance of Dr. Michael Chandross of Sandia National Laboratories with operating the LAMMPS simulation package and advice in preparing the simulated structures. Mr. James Custer† of Muhlenberg College, was supported on this project as an NSF-REU student under CHE-1062840. **CMMI-1131361 and CMMI-1436192**